

# Module 1: Foundations of Analog Circuitry and Diode Applications

This module provides a fundamental and comprehensive introduction to the principles governing analog electronic circuits, with a specific focus on the theory and applications of semiconductor diodes. We will establish the core concepts of electrical circuits, delve into the physics of P-N junctions, and then systematically explore how diodes are utilized in practical applications such as rectification, voltage regulation, and wave-shaping. Each topic will be explained in detail, reinforced with relevant formulas and their derivations, and illustrated through carefully worked-out numerical examples to solidify your understanding.

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## 1.1 Introduction to Analog Circuits

### 1.1.1 Defining Analog Circuits

Analog circuits are a class of electronic circuits designed to process and manipulate continuous, time-varying signals. Unlike digital circuits, which operate on discrete voltage levels representing binary states (e.g., ON/OFF, 0/1), analog circuits handle signals that can assume any value within a given continuous range. These signals are direct representations of physical phenomena, such as sound waves, light intensity, temperature, or pressure, which inherently vary smoothly over time.

For instance, a microphone converts continuous sound pressure variations into an analog electrical voltage. This voltage continuously fluctuates in amplitude and frequency, mirroring the characteristics of the original sound wave.

### 1.1.2 Importance of Analog Circuits

The significance of analog circuits stems from the inherently analog nature of the physical world. Most sensors, transducers, and actuators interact with continuous physical quantities. Before these real-world signals can be processed by digital systems (like microcontrollers or computers) or used to drive analog devices (like motors or loudspeakers), they often require conditioning by analog circuitry. This conditioning can include amplification (increasing signal strength), filtering (removing unwanted noise), modulation, or conversion.

Furthermore, even in a world increasingly dominated by digital technology, analog circuits are indispensable at the interface between the digital and physical domains. Analog-to-digital converters (ADCs) and digital-to-analog converters (DACs), which bridge these two domains, are themselves complex analog circuits.

### 1.1.3 Diverse Applications of Analog Circuits

Analog circuits are the foundational building blocks for an immense variety of electronic systems across numerous industries. Their applications are widespread and critical for the functioning of modern technology. Some prominent examples include:

- **Audio and Communication Systems:**

- **Amplifiers:** Boosting weak audio signals from microphones or musical instruments to drive loudspeakers or headphones.
  - **Radio Frequency (RF) Circuits:** Designing transmitters and receivers for wireless communication (e.g., cellular phones, Wi-Fi, Bluetooth, satellite communication). This involves intricate analog processing for modulation, demodulation, mixing, and filtering of high-frequency signals.
  - **Power Management:**
    - **Power Supplies:** Converting alternating current (AC) from the wall outlet into stable, regulated direct current (DC) required by most electronic devices. This involves rectification, filtering, and voltage regulation.
    - **Battery Charging Circuits:** Managing the charging and discharging cycles of rechargeable batteries.
  - **Sensor Interfacing and Instrumentation:**
    - **Transducer Interfaces:** Converting non-electrical physical quantities (like temperature from a thermistor, pressure from a strain gauge, or light from a photodiode) into measurable electrical signals.
    - **Measurement Equipment:** Building precision instruments like oscilloscopes, multimeters, and spectrum analyzers that measure and display analog waveforms.
  - **Control Systems:**
    - **Motor Control:** Designing circuits to precisely control the speed and direction of electric motors in robotics, industrial automation, and consumer appliances.
    - **Feedback Control:** Implementing closed-loop systems where an output is monitored and fed back to adjust the input, ensuring stability and accuracy (e.g., in aerospace, automotive systems).
  - **Medical Electronics:**
    - **Bio-amplifiers:** Amplifying extremely weak biological signals like electrocardiograms (ECGs) or electroencephalograms (EEGs) for diagnostic purposes.
    - **Medical Imaging:** Circuits for ultrasound, MRI, and X-ray systems.
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## 1.2 Review of Basic Circuit Concepts

A thorough understanding of fundamental circuit laws and principles is absolutely essential before delving into analog component characteristics and circuit analysis. These concepts form the bedrock upon which all complex electronic circuit analysis is built.

### 1.2.1 Ohm's Law

Ohm's Law is a foundational principle that quantifies the relationship between voltage, current, and resistance in an electrical circuit. It states that the current flowing through a conductor between two points is directly proportional to the voltage across the two points and inversely proportional to the resistance between them.

**Formula:** The mathematical expression of Ohm's Law is:  $V = I \times R$

Where:

- V represents the voltage (or potential difference) across the component, measured in **Volts (V)**. Voltage is the electrical potential energy difference per unit charge between two points in a circuit, driving current flow.
- I represents the current flowing through the component, measured in **Amperes (A)**. Current is the rate of flow of electric charge.
- R represents the resistance of the component to the flow of current, measured in **Ohms ( $\Omega$ )**. Resistance is a measure of how much an object opposes the flow of electric current.

**Rearrangements of Ohm's Law:** From the primary formula, we can derive:  $I=V/R$   $R=V/I$

**Numerical Example 1.2.1:** Consider a simple circuit with a 12-volt battery connected across a 240 Ohm resistor.

- **Problem:** Calculate the current flowing through the resistor.
- **Given:**  $V=12\text{ V}$ ,  $R=240\Omega$
- **Applying Ohm's Law:**  $I=V/R$
- **Calculation:**  $I=12\text{ V}/240\Omega=0.05\text{ A}$
- **Result:** The current flowing through the resistor is 0.05 Amperes, or 50 milliamperes (mA).

**Numerical Example 1.2.2:** A light bulb draws a current of 0.2 Amperes when connected to a 1.5 Volt AA battery.

- **Problem:** What is the effective resistance of the light bulb filament?
- **Given:**  $I=0.2\text{ A}$ ,  $V=1.5\text{ V}$
- **Applying Ohm's Law:**  $R=V/I$
- **Calculation:**  $R=1.5\text{ V}/0.2\text{ A}=7.5\Omega$
- **Result:** The resistance of the light bulb filament is 7.5 Ohms.

### 1.2.2 Kirchhoff's Laws

Kirchhoff's Laws are fundamental for analyzing more complex circuits, especially those with multiple sources or parallel paths. They are based on the conservation principles of charge and energy.

**1.2.2.1 Kirchhoff's Current Law (KCL)** KCL states that for any node (or junction) in an electrical circuit, the sum of all currents entering that node must be equal to the sum of all currents leaving that node. This is a direct consequence of the principle of conservation of electric charge, meaning that charge cannot accumulate at a node.

**Formula:**  $\sum I_{\text{entering}} = \sum I_{\text{leaving}}$  Alternatively, the algebraic sum of currents at any node in a circuit is zero:  $\sum I_{\text{node}} = 0$  (where currents entering are positive, and currents leaving are negative, or vice versa).

**Explanation:** Imagine a water pipe junction. The total amount of water flowing into the junction per second must equal the total amount of water flowing out of the junction per second. Similarly, in an electrical node, no charge can be created or destroyed, nor can it accumulate indefinitely.

**Numerical Example 1.2.2.1:** Consider a node where three wires meet. Current  $I_1=3$  A is flowing into the node, and current  $I_2=1$  A is flowing out of the node.

- **Problem:** What is the value and direction of current  $I_3$ ?
- **Applying KCL:**  $I_1 + I_{\text{entering\_node}} = I_2 + I_{\text{leaving\_node}}$  Let's assume  $I_3$  is entering the node initially.  $3\text{ A} + I_3 = 1\text{ A}$   $I_3 = 1\text{ A} - 3\text{ A} = -2\text{ A}$
- **Result:** The negative sign indicates that our initial assumption for  $I_3$ 's direction was incorrect. Therefore,  $I_3$  is actually flowing *out* of the node with a magnitude of 2 Amperes. Check:  $3\text{ A (entering)} = 1\text{ A (leaving)} + 2\text{ A (leaving)}$ .  $3\text{ A} = 3\text{ A}$ . KCL holds.

**1.2.2.2 Kirchhoff's Voltage Law (KVL)** KVL states that the algebraic sum of all voltages (voltage drops and voltage rises) around any closed loop in an electrical circuit must be equal to zero. This law is based on the principle of conservation of energy. As you traverse a closed loop, the total energy gained from voltage sources must equal the total energy lost across voltage drops (e.g., resistors).

**Formula:**  $\sum V_{\text{loop}} = 0$  (where voltage rises are positive, and voltage drops are negative, or vice versa) Alternatively, the sum of voltage rises equals the sum of voltage drops around any closed loop:  $\sum V_{\text{rises}} = \sum V_{\text{drops}}$  (around a loop)

**Explanation:** Imagine climbing a mountain and then descending back to your starting point. The total change in your elevation for the entire journey is zero. Similarly, traversing an electrical loop, the net change in potential must be zero.

**Numerical Example 1.2.2.2:** Consider a series circuit with a 20V voltage source and three series resistors:  $R_1=5\Omega$ ,  $R_2=10\Omega$ , and  $R_3=5\Omega$ .

- **Problem:** Verify KVL by calculating the voltage drop across each resistor.
- **Step 1: Calculate total resistance.** In a series circuit,  $R_{\text{total}} = R_1 + R_2 + R_3$   
 $R_{\text{total}} = 5\Omega + 10\Omega + 5\Omega = 20\Omega$
- **Step 2: Calculate total current.** Using Ohm's Law for the entire circuit:  
 $I_{\text{total}} = V_{\text{source}} / R_{\text{total}}$   $I_{\text{total}} = 20\text{ V} / 20\Omega = 1\text{ A}$
- **Step 3: Calculate voltage drop across each resistor.** Using Ohm's Law for each resistor:  $V_1 = I_{\text{total}} \times R_1 = 1\text{ A} \times 5\Omega = 5\text{ V}$   $V_2 = I_{\text{total}} \times R_2 = 1\text{ A} \times 10\Omega = 10\text{ V}$   $V_3 = I_{\text{total}} \times R_3 = 1\text{ A} \times 5\Omega = 5\text{ V}$
- **Step 4: Apply KVL.** Start from the negative terminal of the source and move clockwise:  $-V_{\text{source}} + V_1 + V_2 + V_3 = 0$  (Convention: voltage drops are positive when moving with current, voltage rises are negative)  $-20\text{ V} + 5\text{ V} + 10\text{ V} + 5\text{ V} = 0$   $0 = 0$
- **Result:** KVL is satisfied, confirming that the sum of voltage drops equals the voltage rise provided by the source.

### 1.2.3 Voltage Dividers

A voltage divider is a fundamental circuit configuration used to produce an output voltage that is a fraction of its input voltage. It consists of two or more series resistors, where the output is taken across one of the resistors.

**Formula (for two resistors):** For a series connection of  $R_1$  and  $R_2$  with an input voltage  $V_{\text{in}}$  across the combination, the output voltage  $V_{\text{out}}$  across  $R_2$  is:  $V_{\text{out}} = V_{\text{in}} \times \frac{R_2}{R_1 + R_2}$

### Derivation:

1. In a series circuit, the current ( $I$ ) through both resistors is the same. Using Ohm's Law for the entire series combination:  $I = \frac{V_{in}}{R_1 + R_2}$
2. The voltage across  $R_2$  ( $V_{out}$ ) is given by Ohm's Law:  $V_{out} = I \times R_2$
3. Substitute the expression for  $I$  from step 1 into step 2:  $V_{out} = \frac{V_{in} \times R_2}{R_1 + R_2}$   
 $V_{out} = V_{in} \times \frac{R_2}{R_1 + R_2}$

**Numerical Example 1.2.3:** A 15V power supply is connected across a voltage divider formed by two resistors:  $R_1 = 4.7 \text{ k}\Omega$  and  $R_2 = 10 \text{ k}\Omega$ .

- **Problem:** Calculate the output voltage across  $R_2$ .
- **Given:**  $V_{in} = 15 \text{ V}$ ,  $R_1 = 4.7 \text{ k}\Omega = 4700\Omega$ ,  $R_2 = 10 \text{ k}\Omega = 10000\Omega$
- **Applying Voltage Divider Formula:**  $V_{out} = 15 \text{ V} \times \frac{10000\Omega}{4700\Omega + 10000\Omega}$   $V_{out} = 15 \text{ V} \times \frac{10000}{14700}$   $V_{out} = 15 \text{ V} \times 0.68027 \approx 10.20 \text{ V}$
- **Result:** The output voltage across  $R_2$  is approximately 10.20 Volts.

### 1.2.4 Current Dividers

A current divider is a circuit configuration that splits the total current entering a parallel combination of resistors into smaller currents flowing through each individual branch. The current in each branch is inversely proportional to the resistance of that branch relative to the total parallel resistance.

**Formula (for two parallel resistors):** For a total current  $I_{total}$  entering a parallel combination of  $R_1$  and  $R_2$ : Current through  $R_1$ :  $I_1 = I_{total} \times \frac{R_2}{R_1 + R_2}$  Current through  $R_2$ :  $I_2 = I_{total} \times \frac{R_1}{R_1 + R_2}$

### Derivation:

1. In a parallel circuit, the voltage ( $V_{parallel}$ ) across both resistors is the same.
2. Using Ohm's Law, the current through  $R_1$  is  $I_1 = \frac{V_{parallel}}{R_1}$ , and the current through  $R_2$  is  $I_2 = \frac{V_{parallel}}{R_2}$ .
3. The total current  $I_{total}$  is the sum of the individual currents:  
 $I_{total} = I_1 + I_2 = \frac{V_{parallel}}{R_1} + \frac{V_{parallel}}{R_2} = V_{parallel} \left( \frac{1}{R_1} + \frac{1}{R_2} \right) = V_{parallel} \left( \frac{R_1 + R_2}{R_1 R_2} \right)$
4. From step 3, we can express  $V_{parallel}$ :  $V_{parallel} = I_{total} \times \frac{R_1 R_2}{R_1 + R_2}$
5. Substitute  $V_{parallel}$  back into the expression for  $I_1$ :  
 $I_1 = \frac{R_2}{R_1} \times \left( I_{total} \times \frac{R_1 R_2}{R_1 + R_2} \right) = I_{total} \times \frac{R_2}{R_1 + R_2}$  Similarly for  $I_2$ :  
 $I_2 = \frac{R_1}{R_1 + R_2} \times \left( I_{total} \times \frac{R_1 R_2}{R_1 + R_2} \right) = I_{total} \times \frac{R_1}{R_1 + R_2}$

**Numerical Example 1.2.4:** A total current of 100 mA enters a parallel combination of two resistors:  $R_1 = 600\Omega$  and  $R_2 = 400\Omega$ .

- **Problem:** Calculate the current flowing through  $R_1$  and  $R_2$ .
- **Given:**  $I_{total} = 100 \text{ mA} = 0.1 \text{ A}$ ,  $R_1 = 600\Omega$ ,  $R_2 = 400\Omega$
- **Applying Current Divider Formula for  $I_1$ :**  $I_1 = 0.1 \text{ A} \times \frac{400\Omega}{600\Omega + 400\Omega} = 0.1 \text{ A} \times \frac{400}{1000} = 0.1 \text{ A} \times 0.4 = 0.04 \text{ A}$   $I_1 = 40 \text{ mA}$
- **Applying Current Divider Formula for  $I_2$ :**  $I_2 = 0.1 \text{ A} \times \frac{600\Omega}{600\Omega + 400\Omega} = 0.1 \text{ A} \times \frac{600}{1000} = 0.1 \text{ A} \times 0.6 = 0.06 \text{ A}$   $I_2 = 60 \text{ mA}$

- **Result:** The current through R1 is 40 mA, and the current through R2 is 60 mA.
  - **Verification (KCL):**  $I_1 + I_2 = 40 \text{ mA} + 60 \text{ mA} = 100 \text{ mA}$ , which equals  $I_{\text{total}}$ . KCL holds.
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### 1.3 Semiconductor Diodes

The diode is one of the simplest and most fundamental semiconductor devices. Its unique ability to allow current flow predominantly in one direction makes it indispensable in countless electronic applications.

#### 1.3.1 P-N Junction Theory: The Heart of the Diode

A semiconductor diode is essentially a P-N junction formed by bringing together two different types of semiconductor materials: a p-type material and an n-type material.

- **P-type Semiconductor:** Created by doping (adding impurities) a pure semiconductor (like silicon) with trivalent atoms (e.g., Boron, Gallium). These dopants create "holes" (absences of electrons) which act as the majority charge carriers. Electrons are minority carriers.
- **N-type Semiconductor:** Created by doping a pure semiconductor with pentavalent atoms (e.g., Phosphorus, Arsenic). These dopants contribute "free" electrons, which act as the majority charge carriers. Holes are minority carriers.

**Formation of the P-N Junction:** When a p-type and an n-type material are joined:

1. **Diffusion:** Due to concentration gradients, majority carriers begin to diffuse across the junction. Electrons from the n-side diffuse into the p-side, and holes from the p-side diffuse into the n-side.
2. **Recombination:** As electrons move into the p-side, they quickly recombine with the holes present there. Similarly, holes moving into the n-side recombine with free electrons.
3. **Depletion Region Formation:** This recombination process near the junction creates a region that is depleted of mobile charge carriers (electrons and holes).
4. **Immobile Ions and Electric Field:** As electrons leave the n-side, they leave behind positively charged donor ions. As holes leave the p-side (or equivalently, electrons from the p-side recombine), they leave behind negatively charged acceptor ions. These fixed, immobile ions create an electric field across the depletion region, directed from the positive ions on the n-side to the negative ions on the p-side.
5. **Barrier Potential (Built-in Voltage,  $V_0$  or  $V_{bi}$ ):** This electric field establishes a potential difference across the depletion region, acting as a natural barrier that opposes further diffusion of majority carriers. This potential difference is called the barrier potential or built-in voltage.
  - For silicon (Si) diodes,  $V_0 \approx 0.7 \text{ V}$  at room temperature.
  - For germanium (Ge) diodes,  $V_0 \approx 0.3 \text{ V}$  at room temperature. This barrier prevents unlimited diffusion and establishes equilibrium in the unbiased diode.

#### 1.3.2 I-V Characteristics: Understanding Diode Behavior

The current-voltage (I-V) characteristic curve graphically illustrates the relationship between the current flowing through a diode ( $I_D$ ) and the voltage applied across its terminals ( $V_D$ ). It reveals three distinct regions of operation:

#### 1.3.2.1 Forward Bias Region:

- **Condition:** The positive terminal of the external voltage source is connected to the p-side (anode) of the diode, and the negative terminal to the n-side (cathode). This connection pushes majority carriers towards the junction.
- **Operation:**
  - When the applied forward voltage ( $V_D$ ) is less than the barrier potential ( $V_0$ ), the external voltage opposes the built-in electric field, but the barrier is not completely overcome. Only a very small current flows (due to minority carriers).
  - As  $V_D$  increases and exceeds the barrier potential (e.g., 0.7 V for Si), the depletion region effectively narrows, and the electric field within it is significantly reduced. This allows majority carriers to easily cross the junction.
  - Current then begins to flow exponentially, increasing rapidly with small increases in  $V_D$ . This voltage at which significant current begins to flow is often called the "knee voltage" or "turn-on voltage" ( $V_{ON}$ ).
- **Current-Voltage Relationship:** The current in forward bias follows an exponential relationship, described by the Shockley Diode Equation (detailed below).

#### 1.3.2.2 Reverse Bias Region:

- **Condition:** The positive terminal of the external voltage source is connected to the n-side (cathode) and the negative terminal to the p-side (anode). This connection pulls majority carriers away from the junction.
- **Operation:**
  - The applied reverse voltage adds to the built-in barrier potential, causing the depletion region to widen.
  - This widened depletion region presents a very high resistance to the flow of majority carriers.
  - Only a very small, almost constant, current flows. This is called the **reverse saturation current ( $I_S$ )** or leakage current. It is primarily due to the flow of minority carriers (electrons generated in the p-side diffusing to the n-side, and holes generated in the n-side diffusing to the p-side) that are swept across the junction by the strong electric field.  $I_S$  is typically in the nanoampere (nA) or picoampere (pA) range for silicon diodes and is highly temperature-dependent.

#### 1.3.2.3 Reverse Breakdown Region:

- **Condition:** If the reverse bias voltage is continuously increased, it eventually reaches a critical point known as the **reverse breakdown voltage ( $V_{BR}$  or  $V_Z$  for Zener diodes)**.
- **Operation:** At  $V_{BR}$ , the electric field in the depletion region becomes extremely strong. This leads to one of two phenomena:

- **Avalanche Breakdown:** Minority carriers gain enough kinetic energy to collide with atoms in the crystal lattice, knocking out additional electrons and creating more electron-hole pairs. These newly generated carriers also gain energy and cause further ionizations, leading to a cascade (avalanche) effect and a rapid, uncontrolled increase in reverse current.
- **Zener Breakdown:** Occurs in heavily doped junctions at lower reverse voltages. The strong electric field directly pulls electrons from their covalent bonds, creating electron-hole pairs.
- **Consequence:** Beyond VBR, the diode effectively loses its ability to block reverse current, and a large current flows with only a slight increase in voltage. If this current is not limited by an external resistor, the excessive power dissipation can permanently damage the diode. Zener diodes are specifically designed to operate safely in this region.

### 1.3.3 Diode Models: From Ideal to Practical

To simplify circuit analysis, diodes are often represented by simplified models. The choice of model depends on the required accuracy and the complexity of the problem.

**1.3.3.1 Ideal Diode Model:** This is the simplest model and is often used for initial conceptual understanding or when the diode drop is negligible compared to other circuit voltages.

- **Forward Bias:** Behaves like a perfect short circuit (zero voltage drop, zero resistance). Current can flow freely.
- **Reverse Bias:** Behaves like a perfect open circuit (infinite resistance, zero current).
- **No Reverse Breakdown:** The model assumes the diode can withstand any reverse voltage.
- **No Power Dissipation:** Ideal diodes consume no power.

**1.3.3.2 Practical Diode Model (Constant Voltage Drop / Piecewise Linear Model):** This model provides a more accurate representation for silicon and germanium diodes by accounting for the forward voltage drop.

- **Forward Bias:** The diode is assumed to be an open circuit until the applied forward voltage ( $V_D$ ) reaches the turn-on voltage ( $V_{ON}$  or  $V_F$ ). Once  $V_D \geq V_{ON}$ , the diode acts like a voltage source of  $V_{ON}$  in series with a small forward resistance ( $r_f$ ). For most general purpose analysis,  $r_f$  is often approximated as zero.
  - $V_{ON} \approx 0.7$  V for Silicon (Si)
  - $V_{ON} \approx 0.3$  V for Germanium (Ge)
- **Reverse Bias:** Behaves as an open circuit (zero current), neglecting the small reverse saturation current and reverse breakdown.

**Numerical Example 1.3.3.2:** A 9V DC source is connected to a series circuit containing a silicon diode and a 220  $\Omega$  resistor.

- **Problem:** Calculate the current flowing through the circuit using the practical diode model ( $V_D = 0.7$  V).
- **Given:**  $V_{source} = 9$  V,  $R = 220\Omega$ ,  $V_D = 0.7$  V
- **Applying KVL (assuming diode is forward biased):**  $V_{source} = V_D + I_D \times R$



- **Calculation:**  $9\text{ V} = 0.7\text{ V} + I_D \times 220\Omega$   $I_D \times 220\Omega = 9\text{ V} - 0.7\text{ V}$   $I_D \times 220\Omega = 8.3\text{ V}$   $I_D = 8.3\text{ V} / 220\Omega \approx 0.0377\text{ A}$
- **Result:** The current flowing through the circuit is approximately 37.7 milliamperes (mA).

**1.3.3.3 Exponential Diode Model (Shockley Diode Equation):** This is the most accurate and fundamental model, providing a precise description of the diode's I-V characteristics across its forward bias region. **Formula:**  $I_D = I_S(e^{\eta V_D / V_T} - 1)$

Where:

- $I_D$ : Diode current (A)
- $I_S$ : Reverse saturation current (A). This is the very small leakage current that flows when the diode is reverse biased. It is highly temperature-dependent and device-specific, typically ranging from  $10^{-15}\text{ A}$  to  $10^{-9}\text{ A}$ .
- $V_D$ : Voltage across the diode (V).
- $\eta$  (eta): Ideality factor (or emission coefficient).
  - For germanium diodes,  $\eta \approx 1$ .
  - For silicon diodes,  $\eta$  is typically between 1 and 2, often approximated as 1 for small currents and 2 for larger currents. It accounts for non-ideal effects like recombination within the depletion region.
- $V_T$ : Thermal voltage (V). This is a constant at a given temperature, representing the average thermal energy per unit charge. **Formula for Thermal Voltage:**  $V_T = kT/q$ 
  - $k$ : Boltzmann's constant ( $1.38 \times 10^{-23}\text{ J/K}$ )
  - $T$ : Absolute temperature in Kelvin (K). Convert Celsius to Kelvin:  $T(\text{K}) = T(^{\circ}\text{C}) + 273.15$ .
  - $q$ : Magnitude of elementary charge ( $1.602 \times 10^{-19}\text{ C}$ )

**Calculation of Thermal Voltage at Room Temperature:** At room temperature ( $25^{\circ}\text{C} = 298.15\text{ K}$ ):  $V_T = 1.602 \times 10^{-19}\text{ C} (1.38 \times 10^{-23}\text{ J/K}) \times (298.15\text{ K}) \approx 0.02586\text{ V} \approx 25.86\text{ mV}$

**Explanation of the Exponential Term:** The term  $e^{\eta V_D / V_T}$  describes the exponential increase in forward current once  $V_D$  approaches and exceeds the barrier potential. The "-1" term accounts for the reverse saturation current when  $V_D$  is negative (reverse bias), but its effect is negligible in forward bias when  $V_D \gg \eta V_T$ .

**Numerical Example 1.3.3.3:** A silicon diode has a reverse saturation current  $I_S = 10\text{ nA}$  ( $10 \times 10^{-9}\text{ A}$ ) and an ideality factor  $\eta = 2$ . Assume room temperature, so  $V_T = 25.86\text{ mV}$ .

- **Problem:** Calculate the diode current  $I_D$  when the forward voltage  $V_D = 0.6\text{ V}$ .
- **Given:**  $I_S = 10^{-8}\text{ A}$ ,  $\eta = 2$ ,  $V_T = 0.02586\text{ V}$ ,  $V_D = 0.6\text{ V}$
- **Applying Shockley Diode Equation:**  $I_D = I_S(e^{\eta V_D / V_T} - 1)$   
 $I_D = (10 \times 10^{-9})(e^{2 \times 0.02586 \times 0.6} - 1)$   $I_D = (10 \times 10^{-9})(e^{0.05172 \times 0.6} - 1)$   
 $I_D = (10 \times 10^{-9})(e^{11.60} - 1)$   $e^{11.60} \approx 109100$   $I_D = (10 \times 10^{-9})(109100 - 1)$   
 $I_D \approx (10 \times 10^{-9}) \times 109099 \approx 0.00109\text{ A}$
- **Result:** The diode current is approximately 1.09 milliamperes (mA). This example highlights the exponential behavior: a small change in  $V_D$  would lead to a large change in  $I_D$ .

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## 1.4 Diode Rectifiers

Rectifiers are electronic circuits that convert alternating current (AC) into pulsating direct current (DC). Diodes are the essential components in rectifiers due to their unidirectional current conduction property, allowing current to flow only in one direction.

### 1.4.1 Half-Wave Rectifier

**Principle of Operation:** A half-wave rectifier utilizes a single diode to allow only one half-cycle (either positive or negative) of the input AC signal to pass through to the load, while blocking the other half-cycle.

**Circuit Configuration:** A basic half-wave rectifier consists of:

1. An AC voltage source (often derived from a transformer secondary winding).
2. A single rectifier diode.
3. A load resistor ( $R_L$ ).

**Detailed Operation:** Let's consider an AC input voltage  $V_{in} = V_m \sin(\omega t)$ , where  $V_m$  is the peak input voltage.

- **During the Positive Half-Cycle ( $0$  to  $\pi$  radians of the input sine wave):**
  - The anode (p-side) of the diode becomes positive with respect to the cathode (n-side).
  - If  $V_{in}$  exceeds the diode's turn-on voltage ( $V_D$ , typically  $0.7\text{ V}$  for Si), the diode becomes forward biased and acts like a closed switch (or a  $0.7\text{ V}$  voltage drop).
  - Current flows through the diode and the load resistor  $R_L$ .
  - The output voltage across  $R_L$  ( $V_{out}$ ) will be  $V_{in} - V_D$ .
- **During the Negative Half-Cycle ( $\pi$  to  $2\pi$  radians of the input sine wave):**
  - The anode of the diode becomes negative with respect to the cathode.
  - The diode becomes reverse biased and acts like an open switch (blocking current).
  - Virtually no current flows through the load resistor.
  - The output voltage across  $R_L$  ( $V_{out}$ ) will be approximately  $0\text{ V}$  (or a very small leakage current related voltage).

**Output Waveform:** The output waveform across the load resistor is a pulsating DC signal, consisting of only the positive (or negative, depending on diode orientation) half-cycles of the input AC sine wave.

### Performance Parameters and Formulas:

- **Peak Inverse Voltage (PIV):** This is the maximum reverse voltage that the diode must withstand when it is not conducting. For a half-wave rectifier, PIV is approximately equal to the peak input voltage ( $V_m$ ).  $PIV = V_m$  (for ideal diode)  $PIV = V_m$  (for practical diode, during the negative half-cycle, the diode blocks the entire peak input)

- **Peak Output Voltage ( $V_{\text{peak(out)}}$ ):**  $V_{\text{peak(out)}}=V_m-V_D$  (for practical silicon diode)  
 $V_{\text{peak(out)}}=V_m$  (for ideal diode)
- **Average (DC) Output Voltage ( $V_{\text{DC}}$  or  $V_{\text{avg}}$ ):** This is the DC component of the pulsating output waveform.  $V_{\text{DC}}=\pi V_{\text{peak(out)}}$  (Derivation involves integrating the half-sine wave over one period)
- **RMS Output Voltage ( $V_{\text{RMS}}$ ):** The root mean square value of the output voltage.  $V_{\text{RMS}}=2V_{\text{peak(out)}}$  (Derivation involves integrating the square of the half-sine wave over one period and taking the square root)
- **Ripple Factor ( $\gamma$ ):** A dimensionless quantity that indicates the amount of AC ripple (undesirable AC component) present in the DC output. A lower ripple factor signifies a smoother DC output.  $\gamma=\text{DC value of output}/\text{RMS value of AC}$



component  $= (V_{\text{DC}}/V_{\text{RMS}})^2 - 1$  For an unfiltered half-wave rectifier:  $\gamma \approx 1.21$  (or 121%). This high value indicates significant ripple.

- **Rectification Efficiency ( $\eta$ ):** The ratio of DC power delivered to the load to the AC power supplied to the rectifier circuit.  $\eta = P_{\text{AC}}/P_{\text{DC}} = V_{\text{RMS}} \times I_{\text{RMS}} / V_{\text{DC}} \times I_{\text{DC}}$  For an ideal half-wave rectifier without a filter, the maximum theoretical efficiency is approximately 40.6%.  $\eta \approx 40.6\%$

#### Disadvantages of Half-Wave Rectifier:

1. **High Ripple Factor:** The output is highly pulsating, requiring substantial filtering for smooth DC.
2. **Low Efficiency:** Only half of the input AC cycle is utilized, leading to wasted input power.
3. **Transformer Utilization Factor (TUF) is Low:** The transformer is inefficiently used.
4. **DC Saturation of Transformer Core:** If a transformer is used, the DC component flowing through the primary can lead to core saturation, potentially damaging the transformer.

**Numerical Example 1.4.1:** A half-wave rectifier circuit is supplied by a transformer providing 12V RMS (root mean square) at its secondary. The diode is silicon ( $V_D=0.7$  V).

- **Problem:** Calculate the peak output voltage, average DC output voltage, and PIV.
- **Given:**  $V_{\text{RMS(in)}}=12$  V,  $V_D=0.7$  V



- **Step 1: Calculate Peak Input Voltage ( $V_m$ ).**  $V_m = V_{\text{RMS(in)}} \times 2 = 12 \times 1.414 = 16.97$  V
- **Step 2: Calculate Peak Output Voltage ( $V_{\text{peak(out)}}$ ).**  $V_{\text{peak(out)}} = V_m - V_D = 16.97 \text{ V} - 0.7 \text{ V} = 16.27$  V
- **Step 3: Calculate Average DC Output Voltage ( $V_{\text{DC}}$ ).**  $V_{\text{DC}} = V_{\text{peak(out)}} / \pi = 16.27 \text{ V} / 3.14159 \approx 5.18$  V
- **Step 4: Calculate PIV.**  $\text{PIV} = V_m = 16.97$  V
- **Result:** The peak output voltage is 16.27 V, the average DC output voltage is approximately 5.18 V, and the PIV is 16.97 V.

### 1.4.2 Full-Wave Rectifiers

Full-wave rectifiers convert both positive and negative half-cycles of the AC input into a pulsating DC output. This results in a smoother DC output (lower ripple) and higher efficiency compared to half-wave rectifiers. There are two main types: center-tapped and bridge rectifiers.

#### 1.4.2.1 Center-Tapped Full-Wave Rectifier

**Principle of Operation:** This configuration uses a center-tapped transformer to provide two out-of-phase AC voltages and two diodes to rectify both halves of the input AC cycle.

##### Circuit Configuration:

1. A center-tapped transformer with its primary connected to the AC source and its secondary having a tap exactly at the center. This creates two secondary voltages that are 180 degrees out of phase with respect to the center tap. Let  $V_{sm}$  be the peak voltage from either end of the secondary to the center tap.
2. Two rectifier diodes (D1 and D2).
3. A load resistor (RL) connected between the center tap and the common point of the diode cathodes.

##### Detailed Operation:

- **During the Positive Half-Cycle of the Input AC ( $V_{in}$ ):**
  - The upper end of the transformer secondary (connected to D1) becomes positive with respect to the center tap, while the lower end (connected to D2) becomes negative.
  - Diode D1 is forward biased (if  $V_{in} > V_D$ ) and conducts.
  - Diode D2 is reverse biased and acts as an open circuit.
  - Current flows from the upper secondary, through D1, through RL (from top to bottom), and back to the center tap.
- **During the Negative Half-Cycle of the Input AC ( $V_{in}$ ):**
  - The upper end of the transformer secondary becomes negative, and the lower end becomes positive with respect to the center tap.
  - Diode D1 is reverse biased.
  - Diode D2 is forward biased (if  $V_{in} > V_D$ ) and conducts.
  - Current flows from the lower secondary, through D2, through RL (from top to bottom, in the *same direction* as D1's current), and back to the center tap.

**Output Waveform:** The output waveform is a pulsating DC signal with positive pulses appearing during both half-cycles of the input. The ripple frequency is twice the input frequency ( $2f_{in}$ ), making it easier to filter.

##### Performance Parameters and Formulas:

- **Peak Inverse Voltage (PIV):** When one diode is conducting, the other diode is reverse biased. The maximum reverse voltage across the non-conducting diode is

approximately twice the peak secondary voltage of one half winding.  $PIV=2V_{sm}$  (for ideal diode)  $PIV=2V_{sm}-V_D$  (for practical diode)

- **Peak Output Voltage ( $V_{peak(out)}$ ):**  $V_{peak(out)}=V_{sm}-V_D$  (for practical silicon diode)  $V_{peak(out)}=V_{sm}$  (for ideal diode)
- **Average (DC) Output Voltage ( $V_{DC}$  or  $V_{avg}$ ):**  $V_{DC}=\pi/2 \times V_{peak(out)}$
- **Ripple Factor ( $\gamma$ ):** For an unfiltered full-wave rectifier:  $\gamma \approx 0.482$  (or 48.2%). Significantly lower than half-wave.
- **Rectification Efficiency ( $\eta$ ):** For an ideal full-wave rectifier without a filter, the maximum theoretical efficiency is approximately 81.2%.  $\eta \approx 81.2\%$

#### Advantages of Center-Tapped Rectifier:

1. Higher efficiency than half-wave.
2. Lower ripple factor than half-wave.
3. Outputs occur twice per input cycle, simplifying filtering.

#### Disadvantages of Center-Tapped Rectifier:

1. Requires a more expensive and often larger center-tapped transformer.
2. Each diode must withstand a high PIV ( $2V_{sm}$ ).

**Numerical Example 1.4.2.1:** A center-tapped full-wave rectifier uses a transformer that provides 15V RMS across each half of its secondary winding (i.e.,  $V_{RMS(sm)}=15$  V). The diodes are silicon ( $V_D=0.7$  V).

- **Problem:** Calculate the peak output voltage, average DC output voltage, and PIV.
- **Given:**  $V_{RMS(sm)}=15$  V,  $V_D=0.7$  V
- **Step 1: Calculate Peak Secondary Voltage (per half winding),  $V_{sm}$ .**



$$V_{sm}=V_{RMS(sm)} \times \sqrt{2} = 15 \text{ V} \times 1.414 = 21.21 \text{ V}$$

- **Step 2: Calculate Peak Output Voltage ( $V_{peak(out)}$ ).**  $V_{peak(out)}=V_{sm}-V_D=21.21 \text{ V}-0.7 \text{ V}=20.51 \text{ V}$
- **Step 3: Calculate Average DC Output Voltage ( $V_{DC}$ ).**  $V_{DC}=2 \times V_{peak(out)} / \pi = 2 \times 20.51 \text{ V} / 3.14159 \approx 13.05 \text{ V}$
- **Step 4: Calculate PIV.**  $PIV=2V_{sm}=2 \times 21.21 \text{ V}=42.42 \text{ V}$
- **Result:** The peak output voltage is 20.51 V, the average DC output voltage is approximately 13.05 V, and the PIV is 42.42 V.

#### 1.4.2.2 Full-Wave Bridge Rectifier

**Principle of Operation:** The bridge rectifier configuration uses four diodes to convert both halves of the input AC cycle into pulsating DC. It eliminates the need for a center-tapped transformer.

#### Circuit Configuration:

1. An AC voltage source (from a transformer secondary or directly from the mains).
2. Four rectifier diodes ( $D_1, D_2, D_3, D_4$ ) arranged in a bridge.

3. A load resistor ( $R_L$ ).

#### Detailed Operation:

- **During the Positive Half-Cycle of the Input AC:**
  - Let the top terminal of the AC source be positive and the bottom terminal be negative.
  - Diodes D1 and D2 are forward biased and conduct (if  $V_{in} > 2V_D$ ).
  - Diodes D3 and D4 are reverse biased.
  - Current flows from the top terminal, through D1, through  $R_L$  (from left to right, assuming standard connection), through D2, and back to the bottom terminal of the source.
- **During the Negative Half-Cycle of the Input AC:**
  - The bottom terminal of the AC source becomes positive, and the top terminal becomes negative.
  - Diodes D3 and D4 are forward biased and conduct.
  - Diodes D1 and D2 are reverse biased.
  - Current flows from the bottom terminal, through D3, through  $R_L$  (from left to right, in the *same direction* as in the positive half-cycle), through D4, and back to the top terminal of the source.

**Output Waveform:** The output waveform is identical to that of the center-tapped full-wave rectifier: a pulsating DC signal with positive pulses appearing during both half-cycles of the input, and a ripple frequency of  $2f_{in}$ .

#### Performance Parameters and Formulas:

- **Peak Inverse Voltage (PIV):** When two diodes are conducting (e.g., D1 and D2), the two non-conducting diodes (D3 and D4) are reverse biased. The voltage across each non-conducting diode is approximately the peak input voltage ( $V_m$ ).  $PIV = V_m$  (for ideal diode)  $PIV = V_m - V_D$  (for practical diode, typically less common to express this way, but conceptually, the diode sees the full input peak minus one diode drop if you consider the loop) - More precisely, the PIV is equal to the peak output voltage. Let's stick to  $PIV = V_{peak(out)} + V_D \approx V_m$  for practical purposes in analysis. For the non-conducting diode, it blocks the peak secondary voltage less one diode drop from the conducting path. Therefore, it has to withstand the peak output voltage.  $PIV = V_{peak(out)} = V_m - 2V_D$  (more accurate for the specific diode in breakdown, but commonly simplified to  $V_m$  for practical maximum voltage rating) *A clearer way to understand PIV for Bridge:* Consider the loop with D1 and D3. When D1 is conducting,  $V_{out} = V_m - 2V_D$ . D3 is reverse biased, and the voltage across it is roughly the difference between  $V_m$  and  $V_{out}$ . So,  $PIV = V_m - V_D$ . However, for diode selection, the PIV rating should be greater than  $V_m$ .
- **Peak Output Voltage ( $V_{peak(out)}$ ):** Due to two diodes conducting in series during each half-cycle, there are two diode voltage drops.  $V_{peak(out)} = V_m - 2V_D$  (for practical silicon diodes)  $V_{peak(out)} = V_m$  (for ideal diode)
- **Average (DC) Output Voltage ( $V_{DC}$  or  $V_{avg}$ ):**  $V_{DC} = \frac{\pi}{2} \times V_{peak(out)}$
- **Ripple Factor ( $\gamma$ ):** For an unfiltered bridge rectifier:  $\gamma \approx 0.482$  (same as center-tapped full-wave).

- **Rectification Efficiency ( $\eta$ ):** For an ideal bridge rectifier without a filter, the maximum theoretical efficiency is approximately 81.2% (same as center-tapped full-wave).

#### Advantages of Bridge Rectifier:

1. Does not require a center-tapped transformer, making the transformer smaller, lighter, and less expensive for a given power output.
2. Higher efficiency and lower ripple than half-wave.
3. PIV rating for each diode is half that of the center-tapped rectifier for the same output voltage ( $V_m$  vs  $2V_{sm}$  for the full secondary).

#### Disadvantages of Bridge Rectifier:

1. Requires four diodes, increasing component count.
2. Has two diode voltage drops in series in the conduction path ( $2V_D$ ), which results in a slightly lower output voltage and slightly more power loss compared to a center-tapped rectifier (which has one diode drop per path).

**Numerical Example 1.4.2.2:** A bridge rectifier circuit is fed by a transformer providing 24V RMS at its secondary. The diodes are silicon ( $V_D=0.7$  V).

- **Problem:** Calculate the peak output voltage, average DC output voltage, and PIV for each diode.
- **Given:**  $V_{RMS(in)}=24$  V,  $V_D=0.7$  V



- **Step 1: Calculate Peak Input Voltage ( $V_m$ ).**  $V_m = V_{RMS(in)} \times 2 = 24 \text{ V} \times 1.414 = 33.94 \text{ V}$
- **Step 2: Calculate Peak Output Voltage ( $V_{peak(out)}$ ).**  $V_{peak(out)} = V_m - 2V_D = 33.94 \text{ V} - 2(0.7 \text{ V}) = 33.94 \text{ V} - 1.4 \text{ V} = 32.54 \text{ V}$
- **Step 3: Calculate Average DC Output Voltage ( $V_{DC}$ ).**  $V_{DC} = 2 \times V_{peak(out)} / \pi = 2 \times 32.54 \text{ V} / 3.14159 \approx 20.71 \text{ V}$
- **Step 4: Calculate PIV for each diode.**  $PIV = V_m - V_D \approx 33.94 \text{ V} - 0.7 \text{ V} = 33.24 \text{ V}$  (approximately, for component selection, typically rated to withstand  $V_m$ )
- **Result:** The peak output voltage is 32.54 V, the average DC output voltage is approximately 20.71 V, and the PIV for each diode is approximately 33.24 V.

## 1.5 Zener Diodes

The Zener diode is a specialized type of diode designed to operate reliably in the reverse breakdown region. Its unique characteristic of maintaining a relatively constant voltage across its terminals, even when the current through it varies significantly, makes it an ideal component for voltage regulation.

### 1.5.1 Breakdown Characteristics of a Zener Diode

Unlike standard rectifier diodes where reverse breakdown is an undesirable phenomenon that can lead to destruction, Zener diodes are specifically manufactured to safely and predictably break down at a precise reverse voltage, known as the **Zener voltage ( $V_Z$ )**.

- **Forward Bias:** In forward bias, a Zener diode behaves like a regular silicon diode, with a forward voltage drop of approximately 0.7 V.
- **Reverse Bias (Before Breakdown):** When reverse biased below its Zener voltage, only a very small reverse leakage current flows, similar to a standard diode.
- **Reverse Breakdown (Zener Region):** As the reverse voltage increases and reaches  $V_Z$ , the diode rapidly starts conducting in the reverse direction. This breakdown occurs due to one of two mechanisms:
  - **Zener Effect:** Dominant in Zener diodes with  $V_Z$  typically below 5.6 V. It involves a strong electric field across the narrow depletion region, directly pulling electrons out of their covalent bonds.
  - **Avalanche Effect:** Dominant in Zener diodes with  $V_Z$  typically above 5.6 V. It involves minority carriers gaining enough energy to collide with other atoms, releasing more carriers in a cascading effect.
  - At approximately 5.6 V, both effects occur simultaneously and tend to cancel each other's temperature coefficients, making 5.6V Zener diodes very stable with temperature variations.
- **Voltage Regulation:** Once breakdown occurs, the voltage across the Zener diode remains remarkably constant at  $V_Z$ , even if the reverse current ( $I_Z$ ) flowing through it changes over a wide range (within its safe operating limits). This constant voltage characteristic is key to its use as a voltage regulator.

### 1.5.2 Voltage Regulation Using Zener Diodes

A Zener diode can be used to stabilize an output voltage despite variations in the input voltage or changes in the load current. This is achieved by connecting the Zener diode in parallel with the load and in series with a current-limiting resistor.

#### Circuit Configuration (Simple Zener Regulator):

1. **Unregulated DC Input Voltage ( $V_{in}$ ):** This voltage is typically from a rectified and filtered power supply, but it may fluctuate.
2. **Series Current-Limiting Resistor ( $R_S$ ):** This resistor is crucial. It limits the current flowing through the Zener diode and the load, protecting the Zener from excessive current when the input voltage is high or the load current is low.
3. **Zener Diode ( $D_Z$ ):** Connected in reverse bias across the load. Its cathode points towards the higher potential.
4. **Load Resistor ( $R_L$ ):** The component(s) that require the regulated voltage.

#### Detailed Operation for Voltage Regulation:

- **Condition for Regulation:** For the Zener diode to regulate, the input voltage  $V_{in}$  must be greater than the Zener voltage  $V_Z$ , and there must be enough current to keep the Zener in its breakdown region ( $I_Z \geq I_{Zmin}$ ).
- **Load Current Variation (Constant Input Voltage):**



- If the load current ( $I_L$ ) decreases (meaning  $R_L$  increases), less current is drawn by the load. Since  $V_Z$  is maintained, the excess current is diverted through the Zener diode ( $I_Z$  increases). The total current through  $R_S$  ( $I_S = I_Z + I_L$ ) remains relatively constant, maintaining the voltage drop across  $R_S$  and thus keeping  $V_{out}$  stable at  $V_Z$ .
- If the load current ( $I_L$ ) increases (meaning  $R_L$  decreases), more current is drawn by the load. The Zener current ( $I_Z$ ) decreases to compensate. As long as  $I_Z$  does not drop below  $I_{Zmin}$ , the Zener remains in breakdown, and  $V_{out}$  remains constant at  $V_Z$ .
- **Input Voltage Variation (Constant Load Current):**
  - If the input voltage ( $V_{in}$ ) increases, the voltage drop across  $R_S$  ( $V_S = V_{in} - V_Z$ ) increases. This causes an increase in the series current ( $I_S$ ). Since  $I_L$  is constant, the excess current flows through the Zener diode ( $I_Z$  increases), absorbing the input voltage fluctuation and keeping  $V_{out}$  stable at  $V_Z$ .
  - If the input voltage ( $V_{in}$ ) decreases, the voltage drop across  $R_S$  decreases, reducing  $I_S$ . Consequently,  $I_Z$  decreases. As long as  $I_Z \geq I_{Zmin}$ ,  $V_{out}$  remains  $V_Z$ .

### Key Formulas for Zener Regulator Design:

1. **Total Series Current ( $I_S$ ):**  $I_S = I_Z + I_L$  (from KCL at the output node)
2. **Voltage Drop across Series Resistor ( $V_S$ ):**  $V_S = V_{in} - V_Z$  (from KVL around the loop)
3. **Calculating Series Resistor ( $R_S$ ):**  $R_S = I_S V_S = I_Z + I_L V_{in} - V_Z$
4. **Load Current ( $I_L$ ):**  $I_L = V_Z / R_L$
5. **Zener Power Dissipation ( $P_Z$ ):**  $P_Z = V_Z \times I_Z$  The maximum Zener current ( $I_{Zmax}$ ) should be calculated based on the maximum power rating ( $P_{Zmax}$ ) of the Zener diode:  $I_{Zmax} = P_{Zmax} / V_Z$ . It is crucial that the calculated  $I_Z$  does not exceed  $I_{Zmax}$  under any operating condition (especially at minimum load and maximum input voltage).

### Design Considerations:

- **Minimum Zener Current ( $I_{Zmin}$ ):** A minimum current must flow through the Zener diode to keep it in the breakdown (regulating) region. This value is usually provided in the Zener diode's datasheet. If  $I_Z$  drops below  $I_{Zmin}$ , regulation will cease.
- **Maximum Zener Current ( $I_{Zmax}$ ):** The Zener current must not exceed the diode's maximum power rating to prevent damage. This typically occurs when  $V_{in}$  is maximum and  $R_L$  is maximum (or open-circuited,  $I_L = 0$ ).
- **Choice of  $R_S$ :**  $R_S$  is typically chosen to ensure that  $I_Z \geq I_{Zmin}$  under worst-case conditions (minimum  $V_{in}$  and maximum  $I_L$ ).
- **Input Voltage Range:** The regulator works effectively only if  $V_{in}$  is consistently above  $V_Z$ .

**Numerical Example 1.5.2 (Zener Regulator Design):** Design a Zener voltage regulator to provide a stable 6.8V output for a load that draws current from 0 mA (no load) to 40 mA (full load). The unregulated input voltage varies from 10V to 14V. The Zener diode chosen has  $V_Z = 6.8$  V,  $I_{Zmin} = 2$  mA, and a maximum power dissipation  $P_{Zmax} = 1$  W.

- **Step 1: Calculate  $I_{Zmax}$  for the chosen Zener diode.**  $I_{Zmax}=P_{Zmax}/V_Z=1\text{ W}/6.8\text{ V}\approx 0.147\text{ A}=147\text{ mA}$ . This is the absolute maximum current the Zener can handle.
  - **Step 2: Determine  $R_S$ .** The resistor  $R_S$  must be chosen such that the Zener remains in breakdown even at the worst-case condition (when  $V_{in}$  is minimum and  $I_L$  is maximum). At  $V_{in(min)}=10\text{ V}$  and  $I_{Lmax}=40\text{ mA}$ , we need  $I_Z\geq I_{Zmin}=2\text{ mA}$ . So, the current through  $R_S$  under this condition ( $I_S(min)$ ) must be:  $I_S(min)=I_{Zmin}+I_{Lmax}=2\text{ mA}+40\text{ mA}=42\text{ mA}$ . Now, calculate the maximum possible value for  $R_S$ :  
 $R_S(max)=(V_{in(min)}-V_Z)/I_S(min)$   $R_S(max)=(10\text{ V}-6.8\text{ V})/42\text{ mA}=3.2\text{ V}/0.042\text{ A}\approx 76.19\Omega$ . To ensure regulation, we must choose an  $R_S$  value *less than or equal to*  $R_S(max)$ . Let's pick a standard value, for example,  $R_S=68\Omega$ .
  - **Step 3: Verify the Zener current at worst-case maximum (maximum  $V_{in}$  and minimum  $I_L$ ).** When  $V_{in(max)}=14\text{ V}$  and  $I_{Lmin}=0\text{ mA}$  (no load), the current through  $R_S$  will be maximum:  $I_S(max)=(V_{in(max)}-V_Z)/R_S$   $I_S(max)=(14\text{ V}-6.8\text{ V})/68\Omega=7.2\text{ V}/68\Omega\approx 0.10588\text{ A}=105.88\text{ mA}$ . Since  $I_{Lmin}=0$ , all of this current flows through the Zener:  $I_Z=I_S(max)\approx 105.88\text{ mA}$ . *Check if  $I_Z$  exceeds  $I_{Zmax}$ :*  $105.88\text{ mA}<147\text{ mA}$ . The Zener diode is safe under maximum input voltage and no-load conditions.
  - **Result:** A suitable series resistor for this Zener regulator design is  $R_S=68\Omega$ . This ensures the Zener remains in regulation and operates within its safe current limits.
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## 1.6 Special Purpose Diodes (Brief Overview)

Beyond the standard rectifier and Zener diodes, several other diode types are engineered to exploit specific semiconductor properties for specialized functions. While we won't delve into exhaustive detail, a brief understanding of their principles and applications is valuable.

### 1.6.1 Light-Emitting Diodes (LEDs)

- **Principle of Operation:** LEDs are semiconductor devices that emit light when an electric current passes through them in the forward direction. This phenomenon is called electroluminescence. When the diode is forward biased, electrons from the n-type material and holes from the p-type material recombine in the active region of the P-N junction. During this recombination, energy is released in the form of photons (light particles). The color of the emitted light depends on the energy gap of the semiconductor material used.
- **Key Characteristic:** They convert electrical energy directly into light energy, typically with high efficiency.
- **Applications:**
  - Indicator lights on electronic devices.
  - Digital displays (seven-segment displays, dot matrix displays).
  - General illumination (LED light bulbs).
  - Automotive lighting (headlights, taillights).
  - Backlighting for LCD screens.
  - Optical communication (e.g., in fiber optics, remote controls).

### 1.6.2 Photodiodes

- **Principle of Operation:** Photodiodes are light-sensitive semiconductor devices that convert light energy into an electrical current. They are typically operated in reverse bias. When photons (light particles) with sufficient energy strike the P-N junction, they create electron-hole pairs within or near the depletion region. The strong electric field in the reverse-biased depletion region quickly sweeps these newly generated carriers apart, producing a photocurrent that is directly proportional to the intensity of the incident light.
- **Key Characteristic:** They convert light into an electrical current.
- **Applications:**
  - Light detectors and sensors (e.g., in smoke detectors, automatic doors, light meters).
  - Optical communication receivers (converting optical signals back to electrical).
  - Barcode scanners.
  - Solar cells (when operated in photovoltaic mode, generating voltage from light).

### 1.6.3 Varactor Diodes (Varicap Diodes)

- **Principle of Operation:** Varactor diodes are designed to utilize the voltage-dependent capacitance of a reverse-biased P-N junction. In reverse bias, the depletion region acts like the dielectric of a capacitor, and the p and n regions act as the capacitor plates. As the reverse bias voltage across the varactor diode changes, the width of the depletion region changes, which in turn alters the effective capacitance of the junction. A larger reverse bias voltage increases the depletion region width, thus decreasing the capacitance.
- **Key Characteristic:** Their capacitance varies predictably with the applied reverse bias voltage.
- **Applications:**
  - Voltage-controlled oscillators (VCOs): Used to tune the frequency of an oscillator by varying a control voltage.
  - Phase-locked loops (PLLs): Critical for frequency synthesis and demodulation.
  - Frequency modulators (FM).
  - Tunable filters.
  - Automatic frequency control (AFC) circuits in radios and televisions.

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## 1.7 Diode Clipping and Clamping Circuits

These are fundamental wave-shaping circuits that utilize the non-linear characteristics of diodes to modify the shape of an input AC signal.

### 1.7.1 Diode Clipping (Limiting) Circuits

Clipping circuits, also known as limiters, are designed to remove or "clip" portions of an input signal that exceed or fall below a certain predetermined voltage level. They are often used for overload protection, signal reshaping, or extracting specific parts of a waveform.

**General Principle:** The diode conducts when the input voltage reaches a certain threshold (its turn-on voltage,  $V_D$ , plus any bias voltage), effectively shorting out or diverting the excess voltage.

### Types of Clippers:

- **Series Clippers:** The diode is in series with the load. When the diode is forward biased, the signal passes. When it's reverse biased, it blocks the signal.
- **Parallel (Shunt) Clippers:** The diode is in parallel with the load. When the diode is forward biased, it diverts the current away from the load, clipping the output. When it's reverse biased, it acts as an open circuit, allowing the signal to pass to the load.

### Common Configurations:

#### 1. Positive Series Clipper:

- **Purpose:** Clips off the positive peak of the input signal above a specific level.
- **Circuit Concept:** A diode in series with the input, allowing only the negative portion and unclipped positive portion of the signal to pass. If a DC bias voltage is added, the clipping level shifts.
- **Operation Example (Ideal Diode):**
  - If the diode is oriented to pass current when input is positive, but a battery  $V_{bias}$  is in series with the diode opposing conduction:
  - When  $V_{in} < V_{bias}$ , the diode is reverse biased (or not sufficiently forward biased), so no current flows, and  $V_{out} = 0$  (for simple series).
  - When  $V_{in} \geq V_{bias}$ , the diode becomes forward biased and conducts.  $V_{out} = V_{in} - V_{bias}$  (assuming output taken across a resistor after the diode). If output is directly after diode, it just follows input after conduction. More commonly, a diode in series allows only one polarity to pass. A diode in shunt with a battery is used for clipping.

Let's clarify for a practical series clipper example: A diode (anode to input, cathode to output/load) will pass only positive voltages greater than  $V_D$ .  $V_{out} = V_{in} - V_D$  for  $V_{in} > V_D$ , and  $V_{out} = 0$  for  $V_{in} < V_D$ . If a bias voltage is added in series with the diode:  $V_{out} = V_{in} - (V_{bias} + V_D)$  for  $V_{in} > V_{bias} + V_D$ .

#### 2. Positive Parallel (Shunt) Clipper (More common for defined clipping levels):

- **Purpose:** Limits the positive voltage of the output to a specific level.
- **Circuit Concept:** A resistor in series with the input, and a diode in parallel with the output load and a DC bias voltage source. The diode's anode connects to the output/load, and its cathode connects to the positive terminal of the bias voltage (or ground for 0V clip).
- **Operation Example (Practical Silicon Diode,  $V_D = 0.7$  V):**
  - **Clipping Level ( $V_{clip}$ ):** If the cathode is connected to a DC source  $V_{ref}$ , the diode conducts when  $V_{out}$  attempts to exceed  $V_{ref} + V_D$ . So,  $V_{clip} = V_{ref} + V_D$ .
  - **When  $V_{in}$  tries to exceed  $V_{clip}$ :** The diode becomes forward biased, effectively clamping the output voltage to  $V_{clip}$ . The excess voltage is dropped across the series resistor.

- **When  $V_{in}$  is below  $V_{clip}$ :** The diode is reverse biased (acts as open circuit), and the output voltage follows the input (assuming the series resistor and load form a voltage divider, or if the load is high impedance,  $V_{out} \approx V_{in}$ ).

### 3. Negative Parallel (Shunt) Clipper:

- **Purpose:** Limits the negative voltage of the output to a specific level.
- **Circuit Concept:** Similar to the positive parallel clipper, but the diode and bias voltage are reversed. The diode's cathode connects to the output/load, and its anode connects to the negative terminal of the bias voltage (or ground).
- **Clipping Level ( $V_{clip}$ ):** If the anode is connected to a DC source  $-V_{ref}$ , the diode conducts when  $V_{out}$  attempts to go below  $-V_{ref} - V_D$ . So,  $V_{clip} = -V_{ref} - V_D$ .
- **Operation:** When  $V_{in}$  tries to go below  $V_{clip}$ , the diode conducts, clamping the output to  $V_{clip}$ . When  $V_{in}$  is above  $V_{clip}$ , the diode is reverse biased, and the output follows the input.

### 4. Combination Clippers (Two-Level Clippers):

- **Purpose:** Clips both the positive and negative peaks of the input signal.
- **Circuit Concept:** Combines a positive clipper and a negative clipper in parallel across the output. Can use two biased diodes, or two Zener diodes back-to-back.
- **Operation:** One diode clips the positive peak to  $V_{clip1}$ , and the other clips the negative peak to  $V_{clip2}$ . The output is a waveform with its amplitude limited between these two levels.

**Numerical Example 1.7.1 (Positive Parallel Clipper):** An input sinusoidal voltage  $V_{in}(t) = 15\sin(\omega t)$  Volts is applied to a parallel clipper circuit consisting of a  $1\text{ k}\Omega$  series resistor and a silicon diode ( $V_D = 0.7\text{ V}$ ) whose anode is connected to the output node and cathode is connected to a  $+5\text{V}$  DC source. The output is taken across the diode.

- **Problem:** Determine the clipping level and sketch the output waveform.
- **Given:**  $V_{in}(\text{peak}) = 15\text{ V}$ ,  $R_S = 1\text{ k}\Omega$ ,  $V_D = 0.7\text{ V}$ , Bias voltage  $V_{bias} = +5\text{ V}$ .
- **Step 1: Determine the Clipping Level.** The diode will become forward biased and conduct when the voltage at the output node ( $V_{out}$ ) tries to exceed  $V_{bias} + V_D$ .  
 $V_{clip} = V_{bias} + V_D = 5\text{ V} + 0.7\text{ V} = 5.7\text{ V}$ .
- **Step 2: Analyze Output Behavior.**
  - **When  $V_{in} > 5.7\text{ V}$ :** The diode conducts, and it effectively clamps  $V_{out}$  to  $5.7\text{ V}$ . The excess voltage ( $V_{in} - 5.7\text{ V}$ ) is dropped across the  $1\text{ k}\Omega$  series resistor.
  - **When  $V_{in} \leq 5.7\text{ V}$  (during the positive half-cycle, and throughout the negative half-cycle):** The diode is reverse biased (or not sufficiently forward biased) and acts as an open circuit. In this scenario, since the diode is open, the output voltage simply follows the input voltage, assuming no load is drawing significant current. So,  $V_{out} \approx V_{in}$ .
- **Result:** The output waveform will be identical to the input for all values from  $-15\text{V}$  up to  $+5.7\text{V}$ . Any portion of the input sine wave that attempts to exceed  $+5.7\text{V}$  will be clipped, so the positive peak of the output will be limited to  $+5.7\text{V}$ . The output will thus range from  $-15\text{V}$  to  $+5.7\text{V}$ .

### 1.7.2 Diode Clamping (DC Restorer) Circuits

Clamping circuits, also known as DC restorers, are used to shift the DC level of an AC input signal without changing its peak-to-peak amplitude. They essentially "clamp" one peak (either positive or negative) of the input waveform to a specific DC voltage level, often 0V.

**General Principle:** A capacitor charges to the peak voltage of the input signal through a diode during one half-cycle. This stored voltage then acts as a DC bias, shifting the entire waveform up or down.

#### Components:

1. **Capacitor:** Blocks the DC component of the input and stores charge to provide the DC shift.
2. **Diode:** Provides the charging path for the capacitor during one half-cycle and blocks it during the other.
3. **Resistor (Optional/Load):** A parallel resistor across the output is sometimes included to provide a discharge path for the capacitor, preventing the DC level from floating indefinitely. In most ideal analyses, it's assumed the capacitor holds its charge well over the period.
4. **DC Bias Voltage (Optional):** Used to clamp the peak to a specific non-zero voltage level.

#### Types of Clampers:

1. **Negative Clamper (Clamps the positive peak to a reference):**
  - **Purpose:** Shifts the entire input waveform downwards such that its positive peak is clamped to approximately the reference voltage (often 0V or  $V_D$ ).
  - **Circuit Concept:** A capacitor is in series with the input, followed by a parallel diode whose anode is connected to the output/load and cathode to ground (or a positive bias voltage).
  - **Operation (Ideal Diode, 0V reference):**
    - **During the Negative Half-Cycle of Input:** The diode becomes forward biased, allowing the capacitor to charge through the diode to the negative peak voltage of the input ( $V_C \approx V_{\text{peak(in)}}$ ).
    - **During the Positive Half-Cycle of Input:** The diode becomes reverse biased. The capacitor acts like a DC voltage source, adding its charged voltage in series with the input signal. Since the capacitor is charged to  $V_{\text{peak(in)}}$ , the output waveform is shifted downwards by this amount.
    - **Resulting Output:** The positive peak of the output will be approximately 0V. The negative peak of the output will be approximately  $-2 \times V_{\text{peak(in)}}$ . The peak-to-peak amplitude remains the same as the input ( $2 \times V_{\text{peak(in)}}$ ).
2. **Positive Clamper (Clamps the negative peak to a reference):**
  - **Purpose:** Shifts the entire input waveform upwards such that its negative peak is clamped to approximately the reference voltage (often 0V or  $-V_D$ ).
  - **Circuit Concept:** Similar to the negative clamper, but the diode is reversed. The capacitor is in series with the input, followed by a parallel diode whose

cathode is connected to the output/load and anode to ground (or a negative bias voltage).

- **Operation (Ideal Diode, 0V reference):**

- **During the Positive Half-Cycle of Input:** The diode becomes forward biased, allowing the capacitor to charge to the positive peak voltage of the input ( $V_C \approx V_{\text{peak}}(\text{in})$ ).
- **During the Negative Half-Cycle of Input:** The diode becomes reverse biased. The capacitor shifts the waveform upwards.
- **Resulting Output:** The negative peak of the output will be approximately 0V. The positive peak of the output will be approximately  $+2 \times V_{\text{peak}}(\text{in})$ . The peak-to-peak amplitude remains the same.

- 3. **Clamper with Bias:** By adding a DC voltage source in series with the diode, the clamping level can be set to a specific non-zero voltage. For example, a negative clamper with a positive bias voltage  $V_{\text{bias}}$  will clamp the positive peak to  $V_{\text{bias}} + V_D$  (for practical diode).

**Numerical Example 1.7.2 (Negative Clamper):** An input sinusoidal voltage  $V_{\text{in}}(t) = 5\sin(\omega t)$  Volts is applied to a negative clamper circuit using a silicon diode ( $V_D = 0.7 \text{ V}$ ) and a capacitor. No external bias voltage is used (clamped to 0V).

- **Problem:** Determine the range of the output voltage and its peak-to-peak amplitude.
- **Given:**  $V_{\text{in}}(\text{peak}) = 5 \text{ V}$ ,  $V_D = 0.7 \text{ V}$ .
- **Step 1: Capacitor Charging.** During the negative peak of the input ( $V_{\text{in}} = -5 \text{ V}$ ), the diode will be forward biased (its anode will be at  $-5 \text{ V}$  and cathode at ground, assuming output across diode). The capacitor will charge to approximately the peak input voltage less the diode drop, but in a clamper, the capacitor charges to compensate the peak. More accurately for a negative clamper, the capacitor charges to  $V_C = V_{\text{peak}}(\text{in}) - V_D$  during the positive cycle when the diode *could* potentially conduct (which it doesn't in a standard negative clamper's "charging" cycle, the diode conducts on negative peaks when clamped to ground, establishing that voltage). Let's re-evaluate the charging for a standard negative clamper (capacitor then diode with anode to output, cathode to ground). During the negative input peak, say  $V_{\text{in}} = -5 \text{ V}$ . The output will be clamped to  $V_D$  below ground.  $V_{\text{out}} = -V_D = -0.7 \text{ V}$ . The capacitor voltage  $V_C$  will be  $V_C = V_{\text{in}} - V_{\text{out}} = (-5 \text{ V}) - (-0.7 \text{ V}) = -4.3 \text{ V}$ . The capacitor charges with the polarity as shown (positive plate connected to input, negative plate connected to output/diode side). So, it's effectively charged to 4.3 V with the polarity indicated. This logic is slightly confusing. A simpler approach: The diode will conduct on the negative peaks, clamping the output to 0 V (if ideal diode) or  $-V_D$  (if practical diode, when its anode is at 0 V and cathode is at the output). For a negative clamper: The diode conducts when the input goes negative. The capacitor charges up to the peak input voltage ( $V_{\text{peak}}(\text{in})$ ). Let's consider the voltage across the capacitor,  $V_C$ . When  $V_{\text{in}}$  reaches its negative peak ( $-5 \text{ V}$ ), the diode conducts. The output voltage  $V_{\text{out}}$  (across the diode) will be  $-V_D = -0.7 \text{ V}$ . The voltage across the capacitor will be  $V_C = V_{\text{in}} - V_{\text{out}} = (-5 \text{ V}) - (-0.7 \text{ V}) = -4.3 \text{ V}$ . So the capacitor is charged to 4.3 V with its left plate (connected to input) negative and its right plate (connected to diode) positive.

- Step 2: Determine Output Range after Clamping.** Once the capacitor is charged, it acts as a DC voltage source of  $V_C=4.3\text{ V}$  in series with the input, effectively shifting the entire input waveform. The output voltage will be:  $V_{out}=V_{in}-V_C=V_{in}-4.3\text{ V}$ .
  - Maximum output:  $V_{out(max)}=V_{in(max)}-V_C=5\text{ V}-4.3\text{ V}=0.7\text{ V}$ . (This is the voltage to which the positive peak is "clamped" or raised/lowered to relative to ground by the diode action)
  - Minimum output:  $V_{out(min)}=V_{in(min)}-V_C=(-5\text{ V})-4.3\text{ V}=-9.3\text{ V}$ .
- Step 3: Calculate Peak-to-Peak Amplitude.**  $V_{p-p(out)}=V_{out(max)}-V_{out(min)}=0.7\text{ V}-(-9.3\text{ V})=0.7\text{ V}+9.3\text{ V}=10\text{ V}$ . This is the same as the input peak-to-peak amplitude ( $5\text{ V}-(-5\text{ V})=10\text{ V}$ ), confirming that clamping shifts the DC level without changing the signal's swing.
- Result:** The output voltage will range from  $-9.3\text{ V}$  to  $0.7\text{ V}$ . The peak-to-peak amplitude is  $10\text{ V}$ . The positive peak of the input sine wave is effectively clamped to  $0.7\text{ V}$ .